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TitleMicrowave heating systemField of the invention

- 5 The present invention relates to a microwave heating system and a method in a microwave heating system according to the preambles of the independent claims.

Background of the invention

- 10 A microwave heating system for carrying out chemical reactions, and particularly organic synthesis reactions, is an important and well-known technique. Using microwave heating in a very special way makes it possible to increase the reaction rate of chemical reactions by orders of magnitude. The use of microwaves also often leads to higher yield and purity of the final product.

- 15 Microwave assisted chemistry has been used for many years. However, the apparatuses and methods have to a great extent been based upon conventional domestic microwave ovens. Domestic microwave ovens have a multimode cavity and the energy is applied at a fixed frequency at 2450 MHz. The use of single
20 mode cavities have also been reported, see e.g. US-5,393,492 and US-4,681,740.

- Recent developments have led towards different types of apparatuses comprising a microwave generator, a separate applicator for holding the load (or sample) to be treated, and a waveguide leading the generated microwave radiation from the
25 generator and coupling it into the applicator.

- When coupling electromagnetic radiation such as microwaves from a source to an applicator, it is important to match the transmission line impedance and the applicator impedance (with load) in order to achieve a good transfer of power.

- 30 The international patent application WO-00/36880 discloses a microwave apparatus and methods for performing chemical reactions where the apparatus applies one or more semiconductor based microwave generators making the apparatus suitable for parallel processing of chemical compound reactions. The
35 invention disclosed in the WO-publication further relates to methods for heating

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a plurality of samples simultaneously or sequentially, methods for monitoring a microwave heated chemical reaction, and methods where the optimum conditions with respect to parameters, such as frequency and applied power can be determined for the system consisting of the combination of apparatus and chemical compound. The apparatus and method can be used to prepare a large number of compounds in a parallel process, where the compounds do not share common molecular properties. This is possible in a parallel process since the apparatus is capable of coupling the application of the electromagnetic radiation to each compound independently. However, this parallel energy application is not described in detail in the WO-publication.

In US-5,796,080 a microwave apparatus for controlling power levels in individual multiple cells is disclosed. This apparatus is alleged to be useful for concurrently controlling a plurality of chemical reactions from a single microwave source. The power level of the microwave energy to be applied to each sample holder is individually adjustable by dynamic mechanical moderating means arranged close to each sample holder. It is considered that one drawback with this known device is the structural complexity of e.g. the moderating means and cross-talk between the separate channels.

The overall object of the present invention is to achieve a microwave heating system adapted to perform parallel processing of a large number of loads in microwave applicators, where the processing of each load may be individually controlled and optimised.

A more specific object is to achieve an economically feasible and structurally realizable microwave heating system.

Summary of the invention

The above-mentioned objects are achieved by the present invention according to the independent claims.

Preferred embodiments are set forth in the dependent claims.

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The microwave heating system and the method in the microwave heating system may operate simultaneously in the time domain and frequency domain. Heating of individual chemical compounds are to be performed in the frequency domain whilst the whole plurality of, for example 24 compounds, will be performed in the time domain.

Heating a compound in the frequency domain refers to tracking its resonant frequency as it warms up and possibly during its boiling.

- 10 The fact that one power amplifier may be shared by a plurality of applicators means that different temperatures may be controlled for many different chemical reactions in parallel. These may be time multiplexed dedicating each chemical reaction a unique time slot. It has been found by the inventors that continuous microwave heating is not necessary. A chemical reaction requires time to absorb the heat. The microwave power may be switched on and off in the form of pulses, where each pulse envelope has a varying duty cycle. In one preferred embodiment of the system the time slots are of fixed duration so the power levels can vary inside each time slot.
- 15
- 20 The goal of this system is to simultaneously heat as many chemical reactions as possible in the shortest period of time to the lowest cost per sample as possible.

A number of advantages of the microwave heating system according to the present invention are that the whole system will require only one power amplifier and only one microwave signal generator, and there is minimum risk of mutual coupling between the applicators due to the possibility to freely dedicate a specific applicator to a specific time slot.

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30 A great benefit of a computer-controlled microwave heating system is that it can steer all individual chemical reactions independently in power, frequency and time, and it can be programmed to learn from the results of the chemical reactions in order to modify heating profiles.

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Short description of the appended drawings

Figure 1 is a block diagram of the microwave heating system according to the present invention.

5 Figure 2 is a block diagram illustrating the different parts of the microwave system according to a preferred embodiment of the present invention.

Figure 3 illustrates a preferred embodiment of the power amplifier.

Figure 4 illustrates a time frame including heating time slots according to the present invention.

Figure 5 illustrates a number of time frames according to the present invention.

10 Figure 6 shows a ramping sequence of one time slot.

Figure 7 schematically illustrates a microwave heating arrangement comprising four microwave heating system as illustrated in figure 2.

Figure 8 illustrates the microwave heating system according to an alternative embodiment of the present invention.

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Detailed description of preferred embodiments of the invention

Initially a bit more should be said here about the nature of microwave heating. Maximum power is generally only required for a small percentage of the total processing time. Another percentage of the time it will require no power at all.

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As mentioned above, the goal of the present invention is to achieve a system adapted to heat as many individual chemical reactions as possible in the shortest period of time to the lowest cost per sample as possible. There will naturally be a compromise between total process time, number of reactions and power available for heating.

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System equations and heating profiles will determine the maximum dedicated slot time a reaction may be allowed in order for the chemical reaction to be maintained. This will naturally be dependent on the rate of microwave absorption of the chemistry and heating profile parameters can be changed at any time.

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In order to design the system hardware it will be necessary to determine how many power amplifiers will be required. In one preferred embodiment 10

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channels per amplifier are arranged where the amplifier has 50 Watts output at 2.45 GHz. With 10 channels per amplifier this implies a 100ms heating slot time per channel per second. If the amplifier power level is increased more channels may be heated in parallel or the process time reduced.

- 5 Still another preferred embodiment is to arrange as few as 2 channels per power amplifier. This will naturally result in other values of the power level and time slot duration, which generally are dependent on the rate of absorption and heat retention of the chemical reaction concerned. It is worth mentioning here that heating at maximum power is only required at the beginning of the heating
- 10 cycle. As the chemical reaction approaches the desired temperature the rate of heating will normally be reduced.

The overall system will now be described with references to figure 1.

- 15 The microwave heating system comprises of a microwave system 2, microwave applicator matrix 4, a chemical compound container (vial) matrix 6, a control means 8, a graphical user interface (GUI) 10, an output device 12, e.g. a plotter, and a DC power supply 14.
- 20 The complete system may be manually or automatically driven via the graphical user interface (GUI), which will enable the user to manipulate the compound heating profiles.

- The system may be connected via a suitable communications link to other
- 25 computer processing systems in order to further enhance the parallel process.

- With references to figure 2 the microwave system 2 comprises a microwave generator 16, an attenuator means 18, a microwave power amplifier 20, a broadband tuneable filter 22, a circulator 24, a microwave switch 26 connected
- 30 to the applicators 28 in the applicator matrix 4, and a reflected power detector 30.

Above the applicator matrix sits the chemical container (vial) matrix, which inserts into the applicator matrix.

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According to the present invention the multiple channels and its respective applicators will be handled in the time domain and each separate chemical reaction will be heated up in the frequency domain inside its own allocated time slot.

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As indicated by arrows in figure 2 the control means 8 steers through a control signal interface 32 the frequency, power and timing of the microwave output power. It also monitors the individual reaction temperature sensors, monitors the pressure sensors and reads the reflected power level at the detector or any other detector in the system.

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All units in the microwave system 2 may be bussed and driven by the control means 8. Some of the controlling signals shown in figure 2 are:

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- control voltage for the power amplifier 20
- control voltage for the attenuator means 18
- control voltage for the microwave generator 16
- control voltage for the microwave switch 26

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The power amplifier 20 may be mounted in a shielded frame to prevent feedback, coupling and leakage into other circuits. The whole system will be housed in an emission free RF sealed frame with an external electrical interface. The instrument will not radiate microwave or radio frequency interference into the surroundings.

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Due to the fact that the applicators are driven time multiplexed, there is no danger of cross-talk or mutual coupling between the applicators. However, if the system should require more than one power amplifier, then the power amplifiers may need to be well shielded from each other. The control algorithm will maintain that two adjacent applicators fed from different amplifiers are never serviced in the same or adjacent time slots.

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Inside the microwave amplifier the final output stage power transistors may be suitably mounted so that the heat will be conducted away effectively.

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There may be variants of this microwave heating instrument. The primary variant may operate between 2.0 to 3.0 GHz or, if possible due to applicator properties, the narrower ISM band 2.4 to 2.5 GHz. Other variants may operate around 900 MHz , 1300 MHz or 5,6 GHz. Each variant may require a different applicator matrix and a relevant microwave/RF power amplifier 20.

The different parts of the microwave system 2 will be further described in the following.

10

The microwave generator 16

The microwave generator 16 may comprise a frequency synthesizer, for example a phase-locked-loop voltage controlled oscillator (VCO). The desired synthesized frequency is steered by the control means via the control signal interface 32.

15

The microwave generator may generate a low output signal level, which may be normalised by a factory-trimmable attenuator. The signal generator may have good frequency stability ensuring reduced system error in resonant frequency tracking.

20 *Attenuator means 18*

This may be a low level input signal attenuator with minimum insertion loss, which is driven by a single controlling voltage in the range 0 to +5V. Microwave attenuation may be such that the final output signal level may be varied from 50 W to 500 mW (or 100 W to 1 W, respectively).

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The purpose of the variable signal attenuator is:

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1. to produce a low level microwave signal whilst searching for the resonant frequency of the chemical compound to be heated.
2. to produce a variable output power level during the heating process.

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Microwave power amplifier 20

The amplifier consists of several gain matched transistor amplifier stages operating in a class suitable for good efficiency and linearity driven at a low supply voltage.

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Figure 3 is a schematic block diagram of a microwave power amplifier according to a preferred embodiment. The input to the microwave power amplifier 20 is the output from the attenuator. [There are many design methods in which the final output power level may be reached, one such method is now described. The signal is first amplified by a fixed 40 dB to give an output power of 10 Watts at 2.45 GHz. This signal is then split by a power splitter into two equal channels of 5 W. These two channels are then amplified by 7 dB to give an output of 25 W per channel which are then combined at a hybrid power combiner to give a final output power level of 50 W]. For lower frequencies, for example 900 MHz, the output power level may be 100 Watts because of the lower absorption at these lower radio frequencies. The amplifier itself will not have variable output power as this will lead to unwanted mismatch and non-linearity. Instead the input power level is varied before the power amplifier.

20 The input signal may be sufficiently clean, to be free of any spurious content and harmonics to avoid intermodulation products and generation of unwanted spurious output frequencies.

25 The output of the microwave power amplifier may also be sufficiently clean, to have no spurious, no intermodulation products and have minimum phase noise. The overtones generated by the amplifier may be filtered away by the broadband tunable filter placed after the amplifier.

30 The power amplifier utilises switched microwave energy so that the power transistors do not get as hot as if they were switched on continuously. Factors that influence the design of the power amplifier are among others current limiting features, temperature sensitivity and reflected power sensitivity.

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Filter 22

The power amplifier may be followed by a tunable microwave broadband filter with minimum insertion loss over the whole operational frequency bandwidth. The filter is preferably a passive high power microwave tunable broadband cavity
5 filter. An extra filter may be included to give maximum attenuation at higher harmonic frequencies ensuring that the power being reflected from the applicator is in the operational frequency bandwidth and all intermodulation products are discarded.

Circulator 24

10 The microwave signal from the power amplifier will be fed to a high-power magnetic circulator 24 and then transmitted to an applicator. The reflected signal from the applicator is diverted to port three of the circulator, which will then be attenuated to fit inside the linear region of a microwave detector 30 which may be, for example, a Schottky diode detector. The converted DC signal
15 may represent the magnitude of the reflected power.

During the tuning phase (see below) the algorithm will utilise the reflected power detector signal to search for the resonant frequency of the chemical compound load, and during the heating phase (see below) to track the resonant frequency
20 which changes with heating.

Microwave Switch 26

A multi-branch microwave switch will transfer the microwave power to a selected applicator. The number of switched outputs will be decided at system design time depending on how many applicators will be serviced by one amplifier. The
25 switch may consist of, for example, pin-diodes or semiconductor relays.

Controlling software

The controlling software run by the control means may drive a closed-loop control heating algorithm and receive feedback from temperature and pressure sensors at the applicators 28 and the reflected power detector 30. It will set the
30 time slot interval, control the output power level, operate the microwave switch, and steer the frequency synthesizer (VCO).

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Microwave Applicator

The present invention is generally applicable for microwave heating of a plurality of microwave applicators and is primarily directed towards the use of time frames that include a number of time slots where microwave energy is applied to the applicator dedicated to a specific time slot.

5 It has been found advantageous to use a specific dielectric microwave applicator having an elongated shape with an upper end and a lower end. The applicator is provided with a load chamber adapted to receive the chemical load to be heated and extending coaxially, with regard to the centre axis of the applicator, from the
10 upper end to a predetermined distance from the lower end of the applicator. The applicator is further provided with a microwave coupling means, arranged in a lower section of the applicator, where microwave energy is fed to the applicator.

A high degree of microwave coupling into the ceramic applicator may be achieved
15 through selection of the correct coaxial transmission line and correct impedance matching to the transmission line.

One example of microwave applicators where the present invention may be applicable is to be found in the international patent application PCT/SE02/01813 having an international filing date of October 4, 2002, by the
20 same applicant as the present application.

DC Power unit 14

If the system will only require one power amplifier then the DC input power requirement may be less than one kilowatt and will be determined by the power amplifier efficiency.

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The operation of the system will now be described.

Preferably the system operation will be through some graphical user interface (GUI). The system operator may control the heating profiles by setting system
30 parameters and monitor the sensors on the applicators.

Figures 4 and 5 illustrate the basic principle of the present invention.

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According to the present invention each microwave applicator is dedicated a heating time slot in a time frame. A time frame comprises time slots for the applicators to be heated, and during microwave heating, microwave energy is applied to the microwave applicators in its respective time slot, in consecutive
5 time frames. The microwave energy is coupled to the respective microwave applicator by the microwave switch in accordance with time slot control signals from said control means.

Within each time slot the microwave energy is optimised with regard to frequency and power level, by said control means, to the load to be heated by the
10 applicator dedicated to that time slot.

In figures 4 and 5 the different heights of the bars represent different powers in separate time slots. Preferably there may also be a number of additional redundant slots per frame so that extra time may be applied to chemical reactions at the start of the heating phase. In figure 5 is illustrated the inventive
15 optimisation; the microwave energy for the same time slot in consecutive time frames are changed (in this example the power decreases for the last time slot).

According to one preferred embodiment there may be, in each time slot, a ramp-up time, full-power time, ramp-down time (see figure 6). The whole sequence is
20 controlled by the control means.

The power ramping sequence will be as follows:

1. set the attenuator to maximum attenuation.
- 25 2. select the channel at the microwave switch.
3. select the relevant frequency at the microwave generator.
4. switch on the final transistor drain voltage for output power at minimum level.
5. ramp up the power by selecting programmed steps at the attenuator.
- 30 6. continue at the required microwave output power level for a defined time inside the time slot.
7. ramp down the output power.
8. switch off the final transistor drain voltage.
9. de-select the channel at the RF switch.

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The reason for having a power ramping profile inside each time slot is to prevent amplifier overshoot and ringing, and to prevent the creation of harmonic frequencies of the switching frequency. If the switching were purely a square wave this would generate an infinite amount of harmonic frequencies of the switching frequency and a reduction of the main carrier power.

According to another embodiment of the present invention with regard to how the microwave energy is applied within each time slot, the ramp-up time and ramp-down time are made shorter and according to one extreme situation approach zero, i.e. the microwave energy more or less initially reaches its highest power level within each time slot.

According to still another embodiment the microwave energy is adjusted to a lower power level, above zero, during switching compared to the level during the rest of the time slot.

Due to the fact that abrupt high power switching may cause unwanted spurious harmonic power appropriate measures may be taken to avoid unwanted emission.

Heating Control Algorithm

The heating algorithm may preferably be divided up into two different phases, namely some resonant frequency search, followed by heating (with or without tracking the change in resonant frequency).

As an alternative the heating control algorithm may use some preset profile that includes variants of the algorithm that do not use any feedback at all and variants where some simplified feedback is used. In that special case where no feedback is used no measurements are performed during the heating phase and one preset frequency and one power setting may be used.

In the following the above-mentioned two phases of the heating control algorithm will be described.

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Resonant frequency search phase

In this phase the attenuator will be set to its highest attenuation (lowest output power) and the oscillator frequency will be swept up and down once to find the resonant frequency of the chemical compound. After the resonant frequency has been determined it may be stored in a memory of the control means.

Main heating phase

In this phase the microwave heating pulses will be applied to the applicators. The closed-loop control algorithm will calculate in real time the power levels that are required in the individual time slots for each applicator. These power levels may vary over time dependent on e.g. the temperature and pressure feedback measurements.

The control algorithm will monitor the reflected power detector and steer the synthesised frequency of the microwave generator to keep the chemical reaction in resonance. This may be done by maintaining the lowest possible reflection coefficient measured at the reflected power detector. As a chemical compound heats up, its resonant frequency predominantly increases, and as it approaches its boiling point the rate of change of resonance reaches its maximum. After boiling has started the resonant frequency still continues to increase for a small duration of time but the rate of change decreases again. For some chemical compounds this rate of change of resonant frequency can be extremely fast around its boiling point whilst other chemicals are much slower. It is dependent on the Q-value of the resonant circuit of the combination of applicator plus chemical compound plus container vial. This combination presents a certain complex load impedance to the amplifier. For some chemicals there is a high Q-value of resonance whilst others are much more broad banded, depending on the dielectric properties of the compound.

Figure 7 schematically illustrates a microwave heating arrangement comprising four microwave subsystems as illustrated in figure 2. One of the subsystems is indicated by a square with dashed periphery.

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In an alternative embodiment of the present invention, which is schematically illustrated in figure 9, the microwave heating system only includes a microwave generator 16', a power amplifier 20', a microwave switch 26' and at least two
5 microwave applicators 28'. This alternative embodiment may be regarded as a minimum version of a microwave heating system according to the present invention. Also included is a control means (not shown in the figure) adapted to control the microwave generator to generate microwave energy to be applied to the applicators, within time slots in time frames, and also to control the
10 microwave switch. In this embodiment it may be decided in advance that a preset level of microwave energy is applied during a predetermined time and that no feedback from the applicators is used.

The present invention also relates to the use of the microwave heating system, or
15 the microwave heating arrangement as described above, as well as the method in such a system or arrangement for performing chemical reactions and especially for organic synthesis reactions.

The present invention is not limited to the above-described preferred
20 embodiments. Various alternatives, modifications and equivalents may be used. Therefore, the above embodiments should not be taken as limiting the scope of the invention, which is defined by the appending claims.